



Conceptual Design of a Z-Pinch Fusion Propulsion System

Advanced Concepts Office
George C. Marshall Space Flight Center
National Aeronautics and Space Administration

Robert Adams, Ph.D., P.E.



Team Members



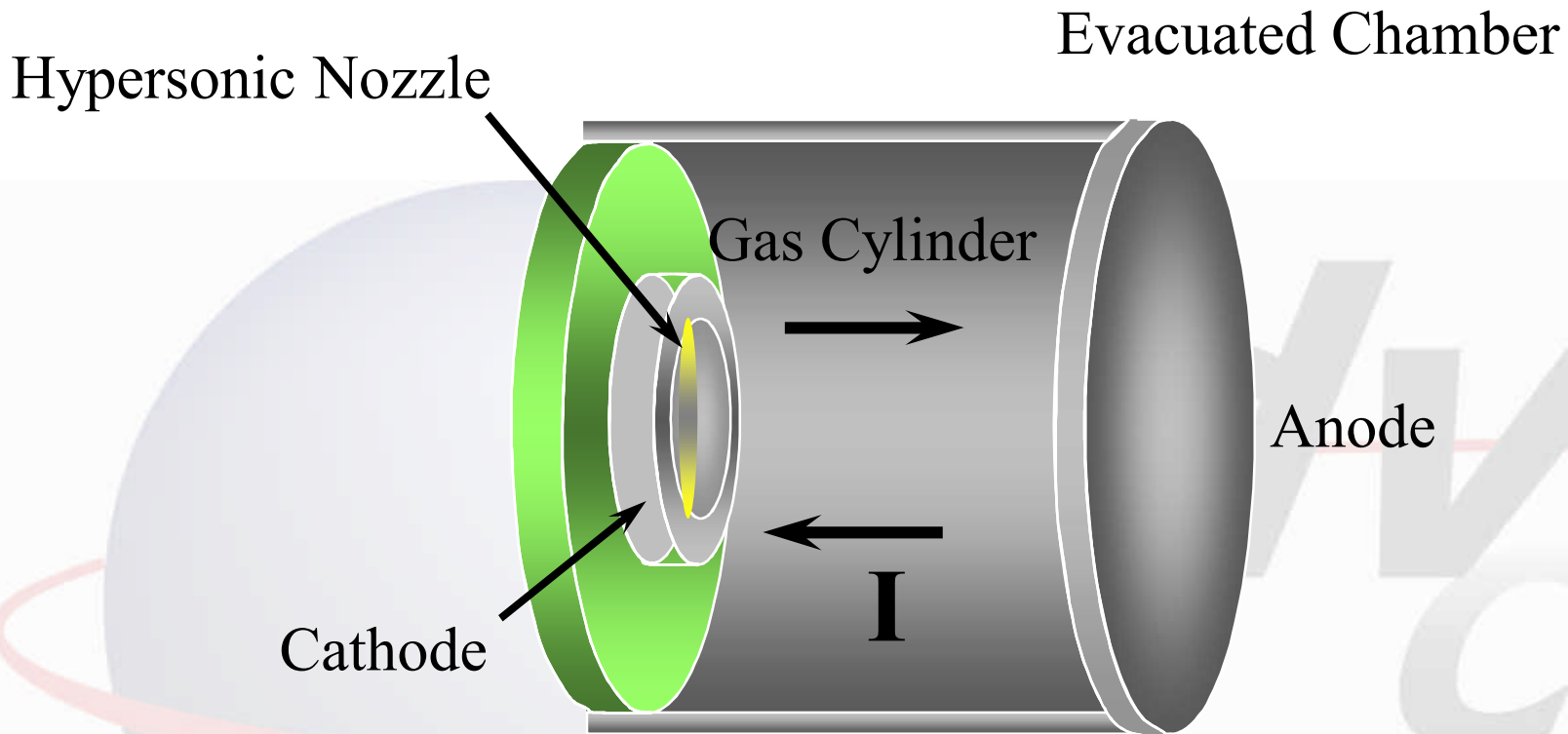
- *Polsgrove T., Adams, R., Fincher, S.* – **NASA (MSFC)**
- *Fabisinski, L.* - **International Space Systems, Inc.**
- *Maples, C.* - **Qualis Corporation**
- *Miernik, J., Statham, G.* - **ERC, Inc.**
- *Cassibry, J., Cortez, R., Turner, M.* - **UAHuntsville**
- *Santarius, J.* - **University of Wisconsin**
- *Percy, T.* - **SAIC, Inc.**



Z-Pinch Fusion: Background

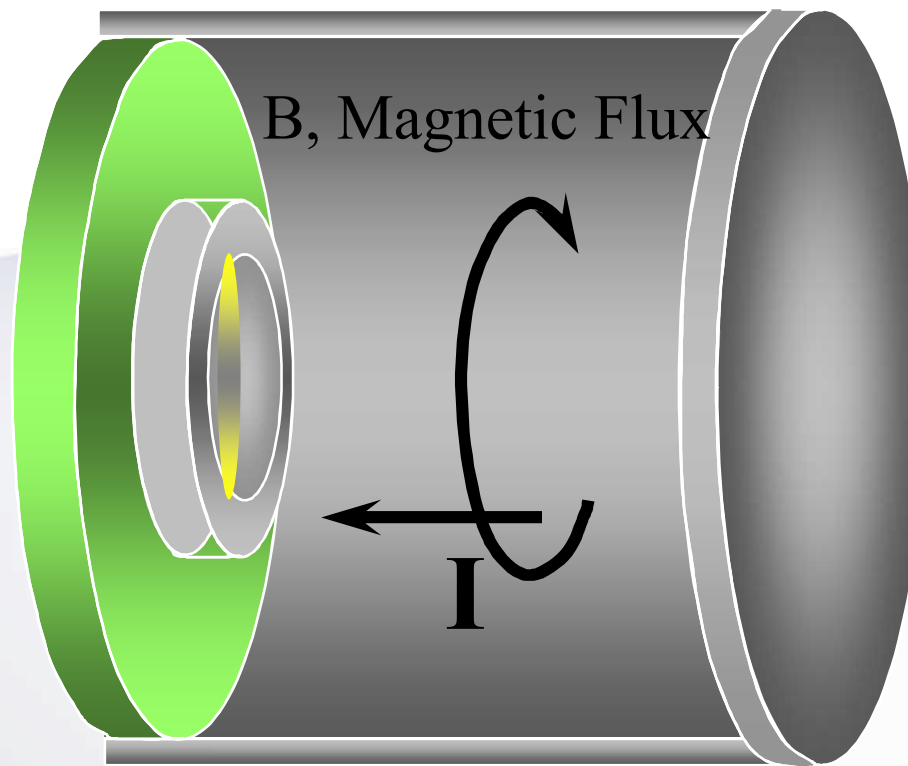


- Nuclear weapon x-rays are simulated through Z-Pinch phenomena.
- New developments at government laboratories is progressing to temperatures capable of causing thermonuclear reactions.
- Such technology could be applied to develop advanced thruster designs that promise high thrust/high specific impulse propulsion
- This project would develop a conceptual design for such a thruster.



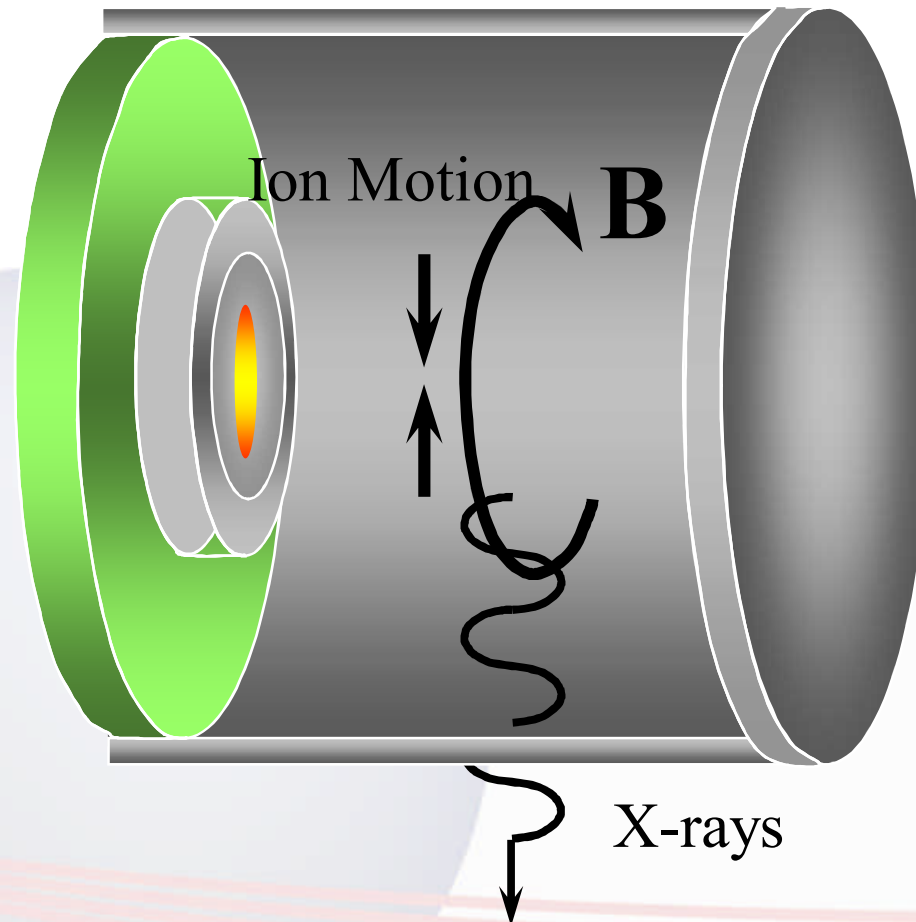


High Current Generates Intense Magnetic Fields





Magnetic Fields Compress the Plasma to X-Ray Temperatures

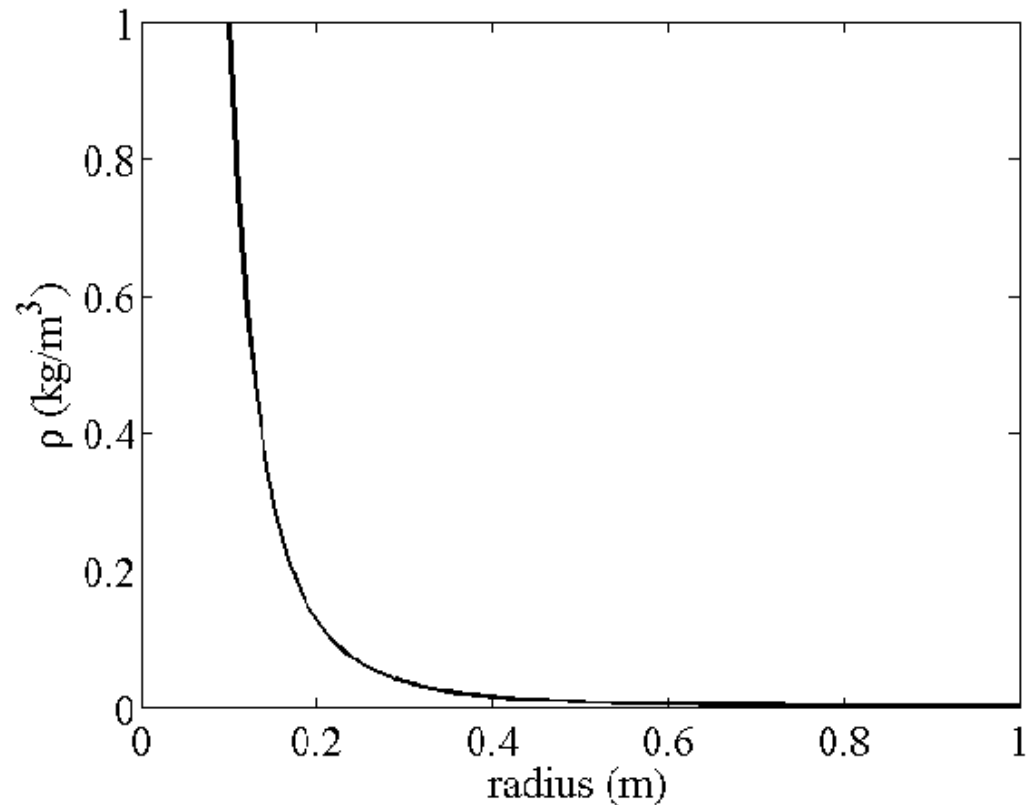




Plasma Instability



- Rayleigh-Taylor is most deleterious effect preventing success, can be overcome with tailored density profile*



*Velikovich, Cochran, and Davis, Phys. Rev. Let. 77(5) 1996.

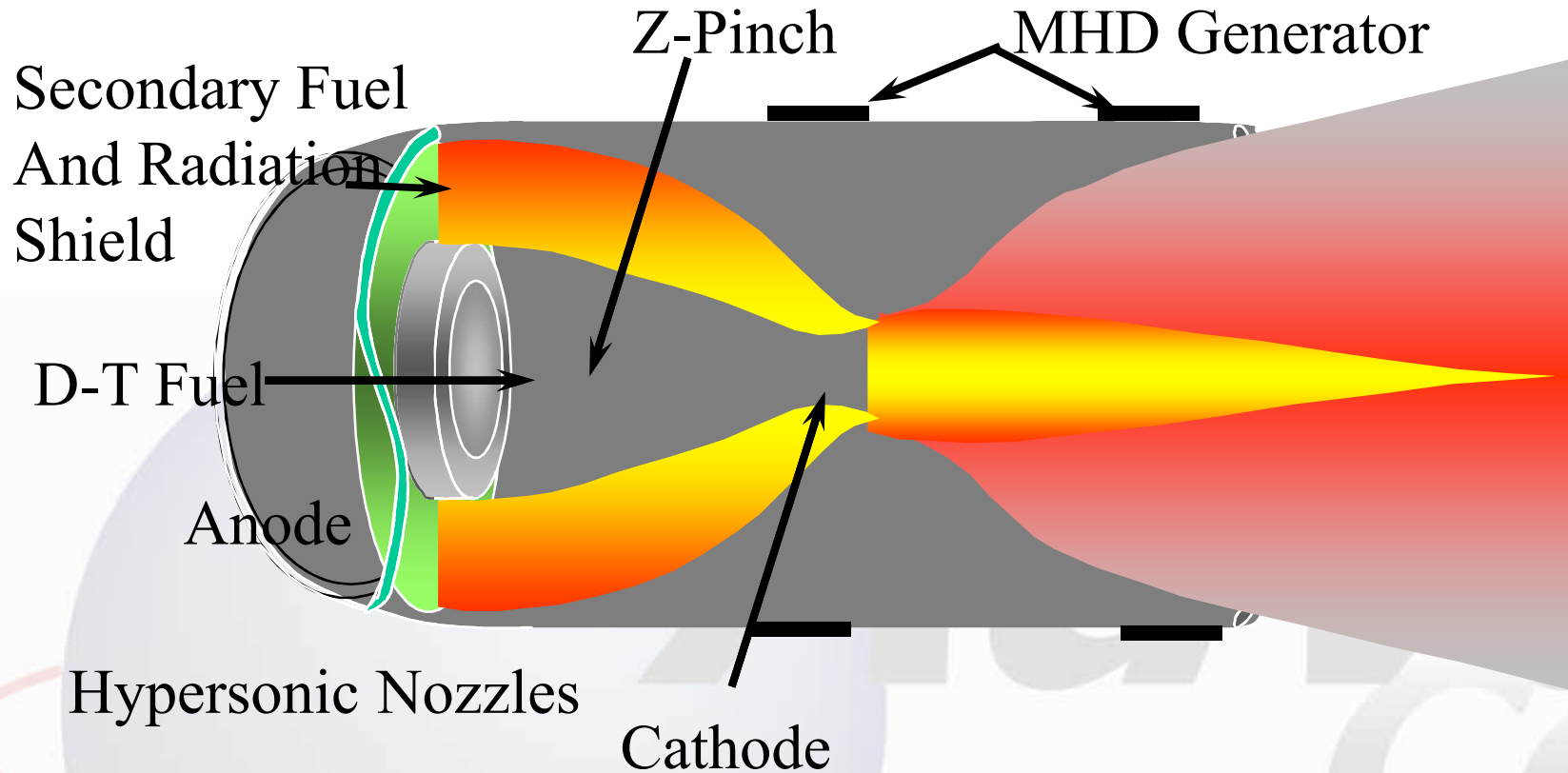


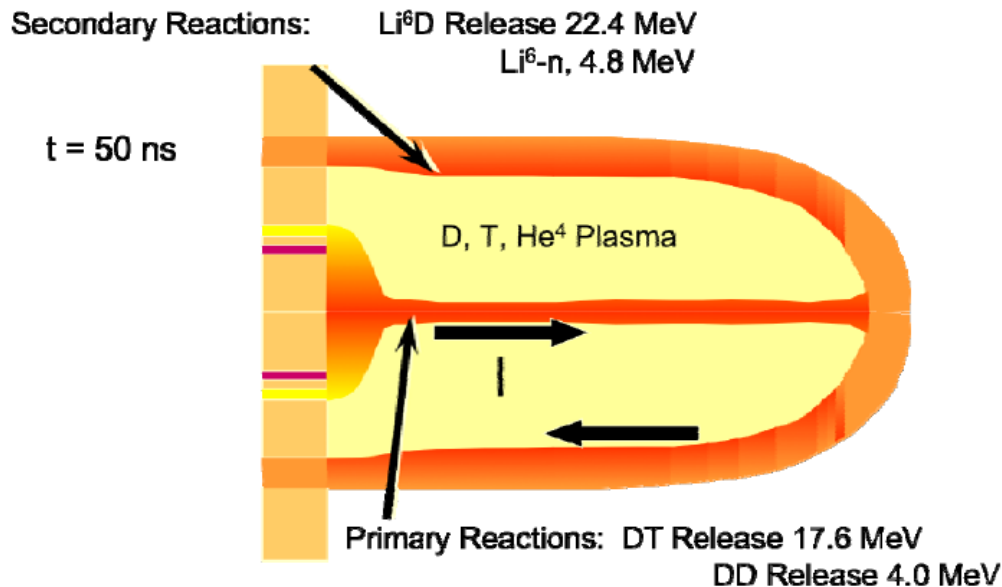
Electrode Erosion



- Coupling electrical energy to plasma
 - Directly coupled devices lead to erosion
 - All susceptible to x-ray radiation and neutron damage
- Potential workarounds
 - Allow electrodes to erode!
 - Consider inductively coupled techniques

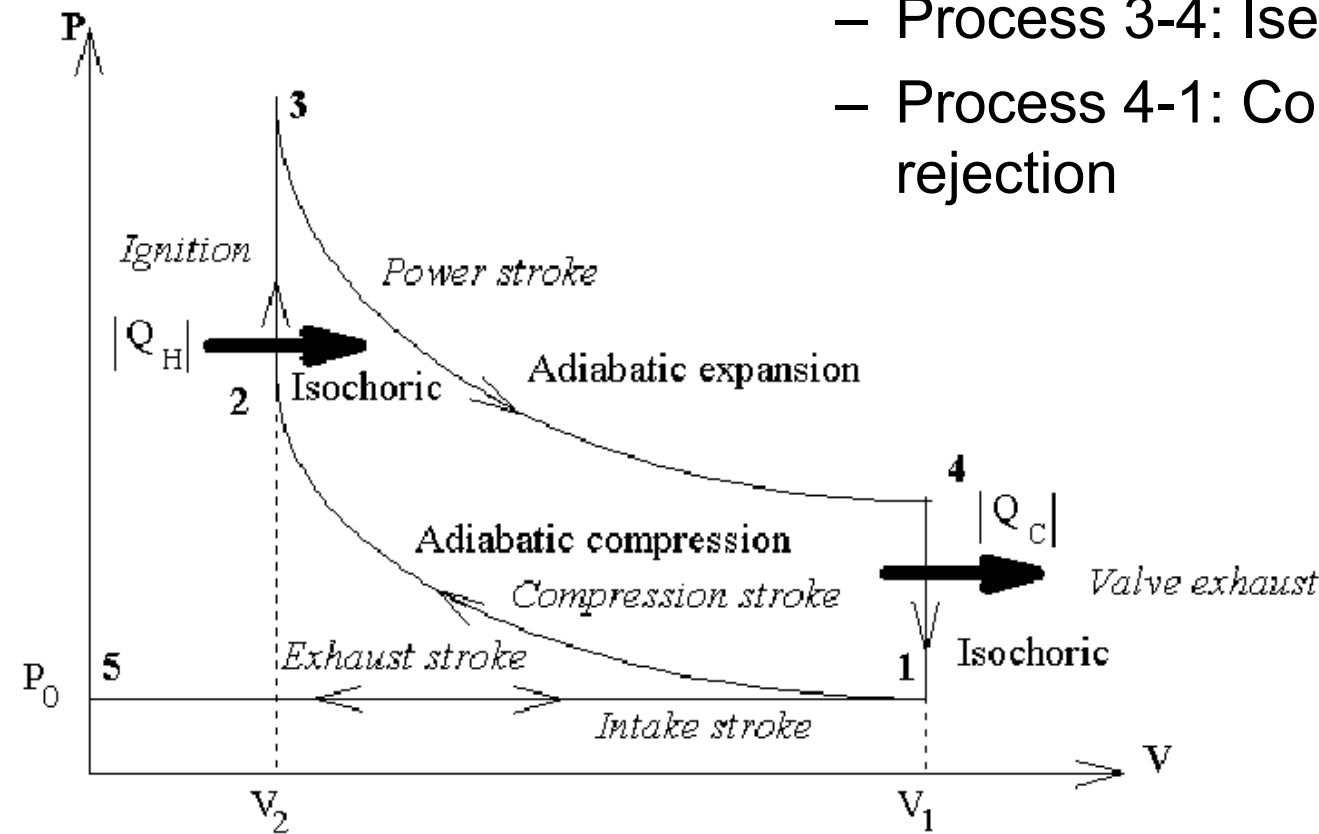






- Annular nozzles with Deuterium-Tritium (D-T) fuel in the innermost nozzle
- Lithium mixture containing Lithium-6/7 in the outermost nozzle.
- The D-T fuel and Lithium-6/7 mixture acts as a cathode

- Treat Z-pinch as Otto cycle
 - Process 1-2: Isentropic compression
 - Process 2-3: Constant volume heat addition
 - Process 3-4: Isentropic expansion
 - Process 4-1: Constant volume heat rejection

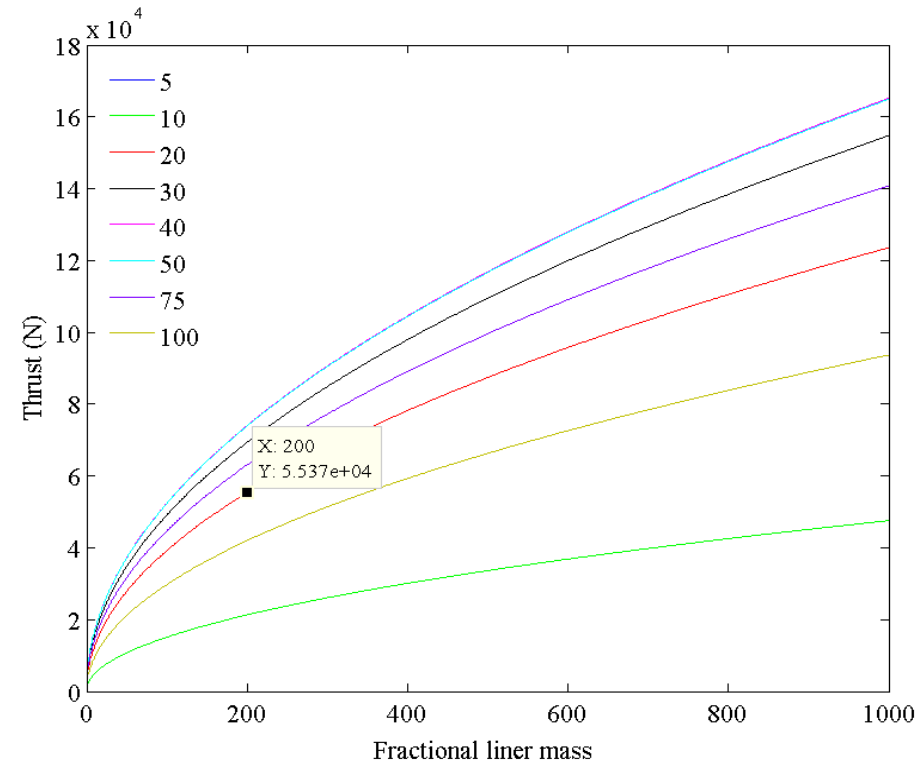
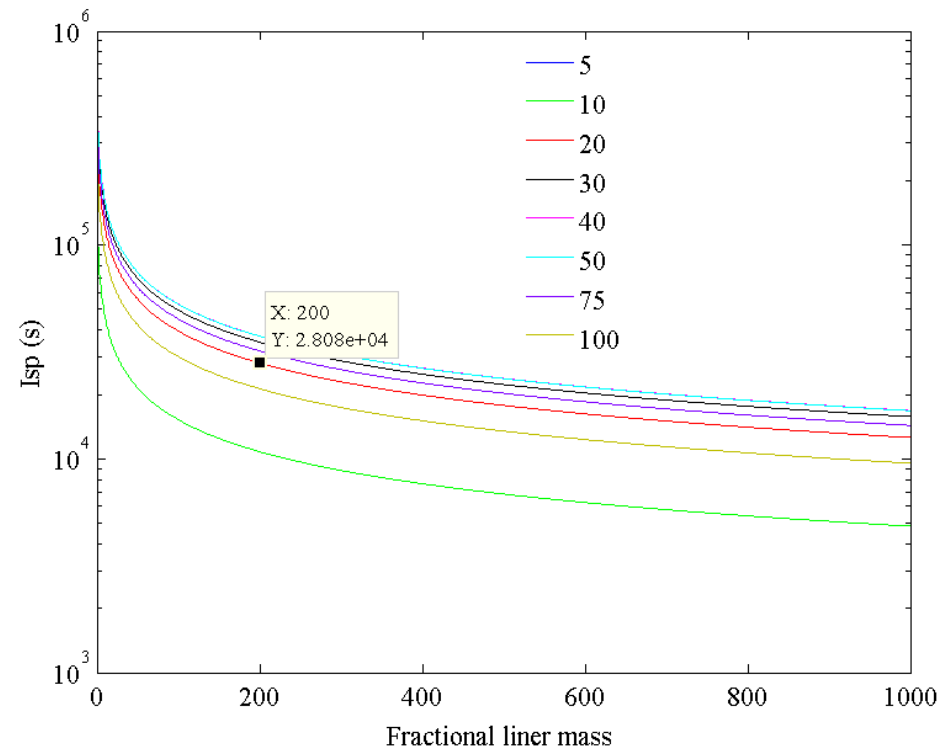




Engine Performance

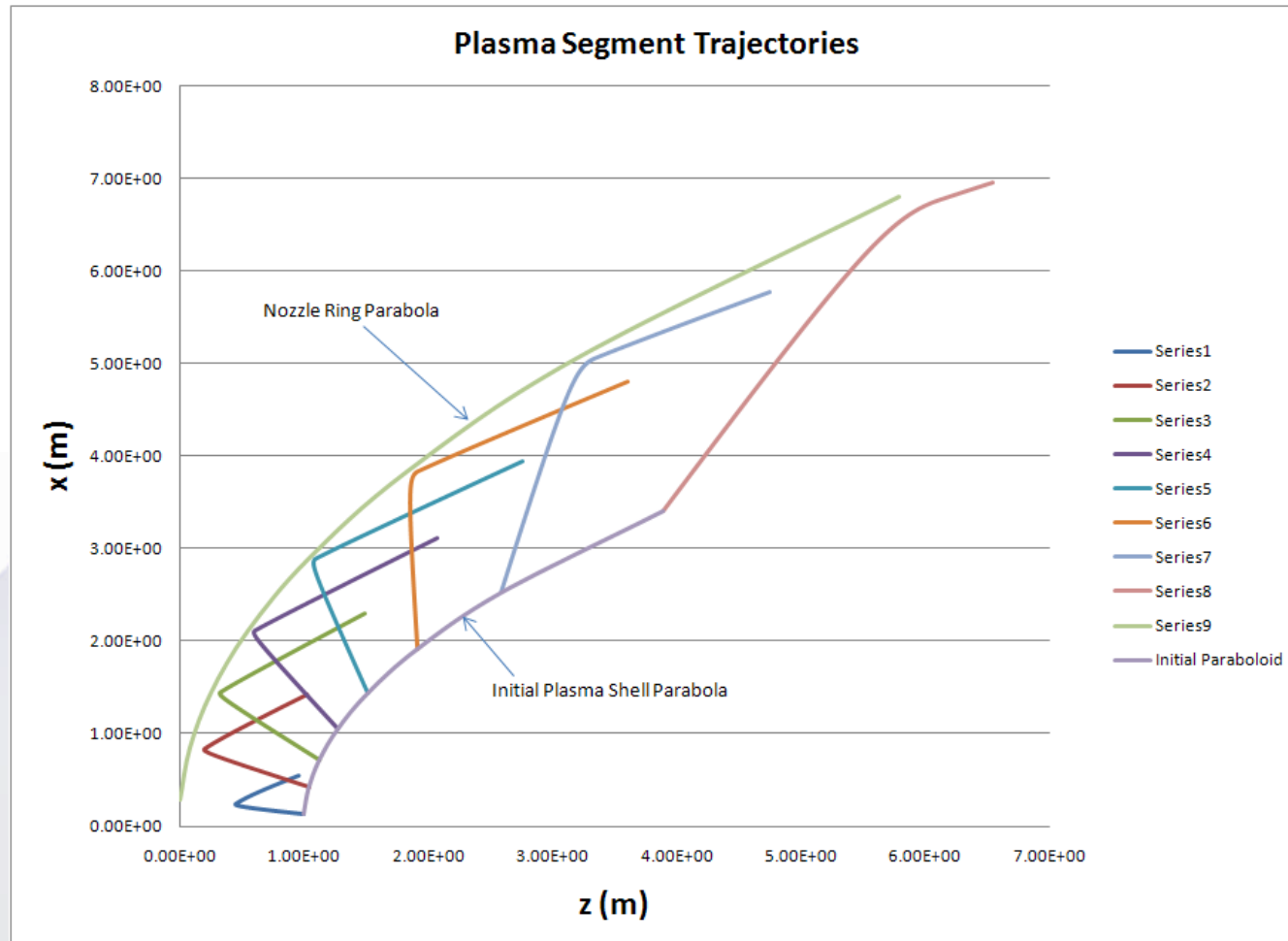


- Engine Performance as a function of liner mass





Nozzle Performance





Mission Analysis



	Mars 90	Mars 30	Jupiter	550 AU
Outbound Trip Time (days)	90.2	39.5	456.8	12936
Return Trip Time (days)	87.4	33.1	521.8	n/a
Total Burn Time (days)	5.0	20.2	6.7	11.2
Propellant Burned (mT)	86.3	350.4	115.7	194.4
Equivalent DV (km/s)	27.5	93.2	36.1	57.2

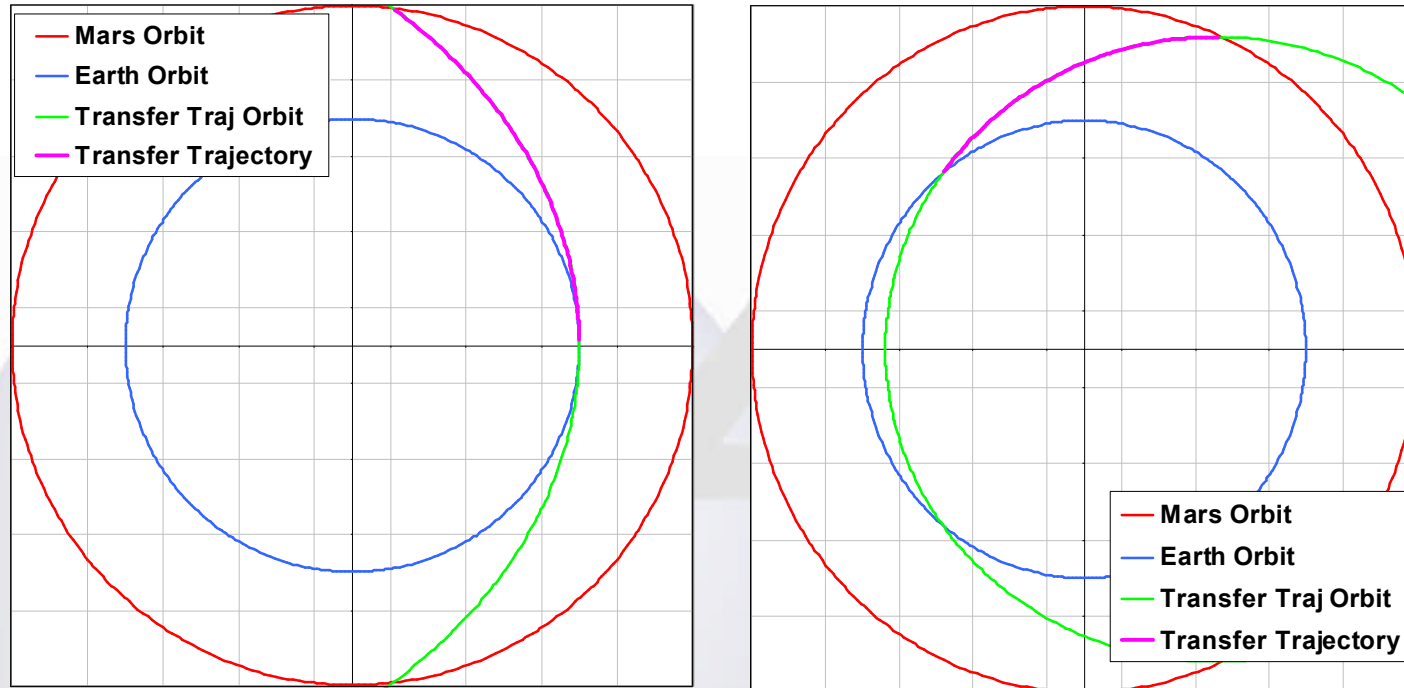
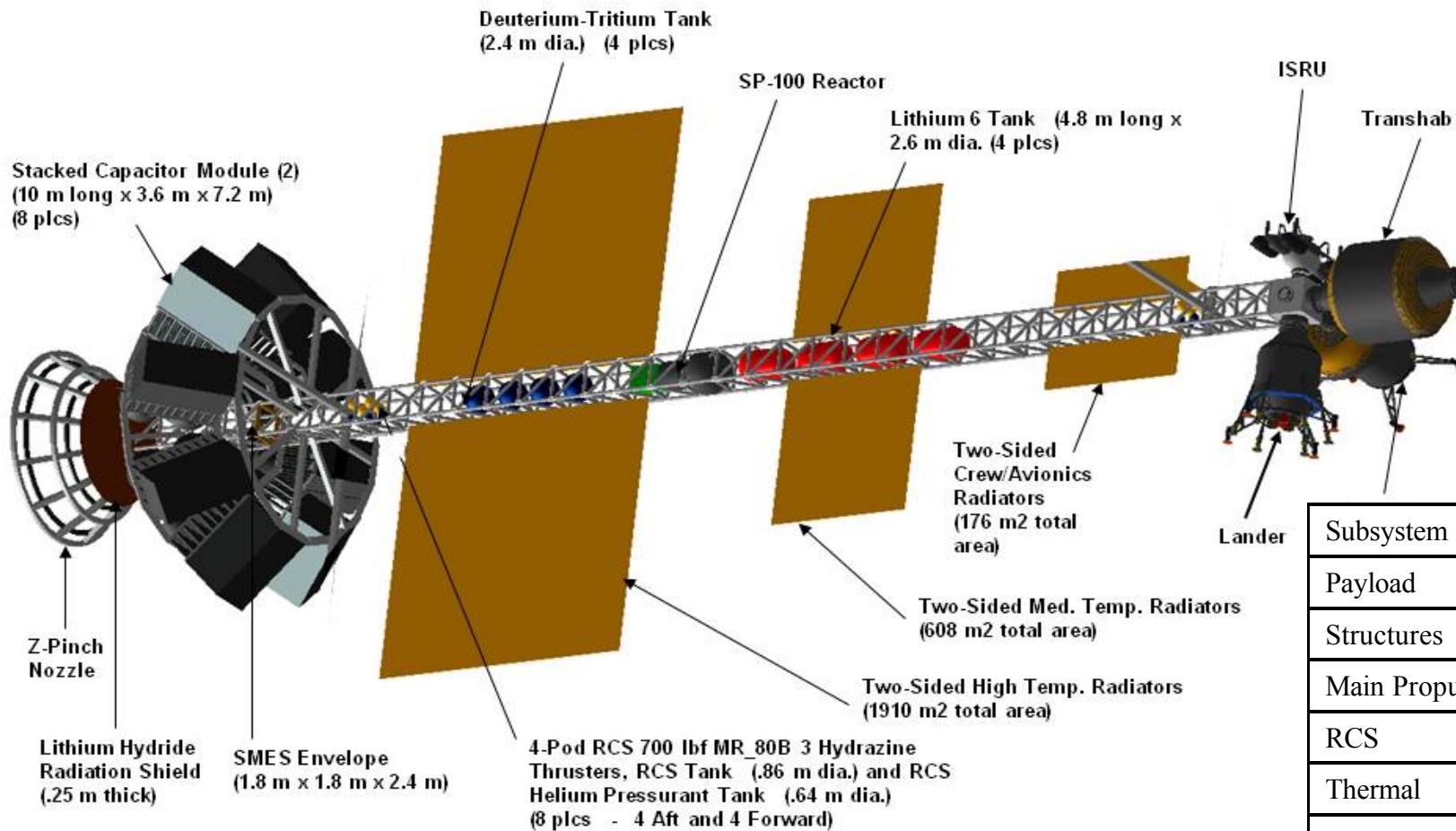


Figure 4.1 Mars 90 Day Transfer Trajectories



Vehicle Configuration



Subsystem	Mass (kg)
Payload	150,000
Structures	54,600
Main Propulsion	95,138
RCS	586
Thermal	77,164
Power	16,480
Avionics	389
Total Dry Mass	394357
30% MGA	73,307
Total Mass	467,664



Thrust Coil Configuration

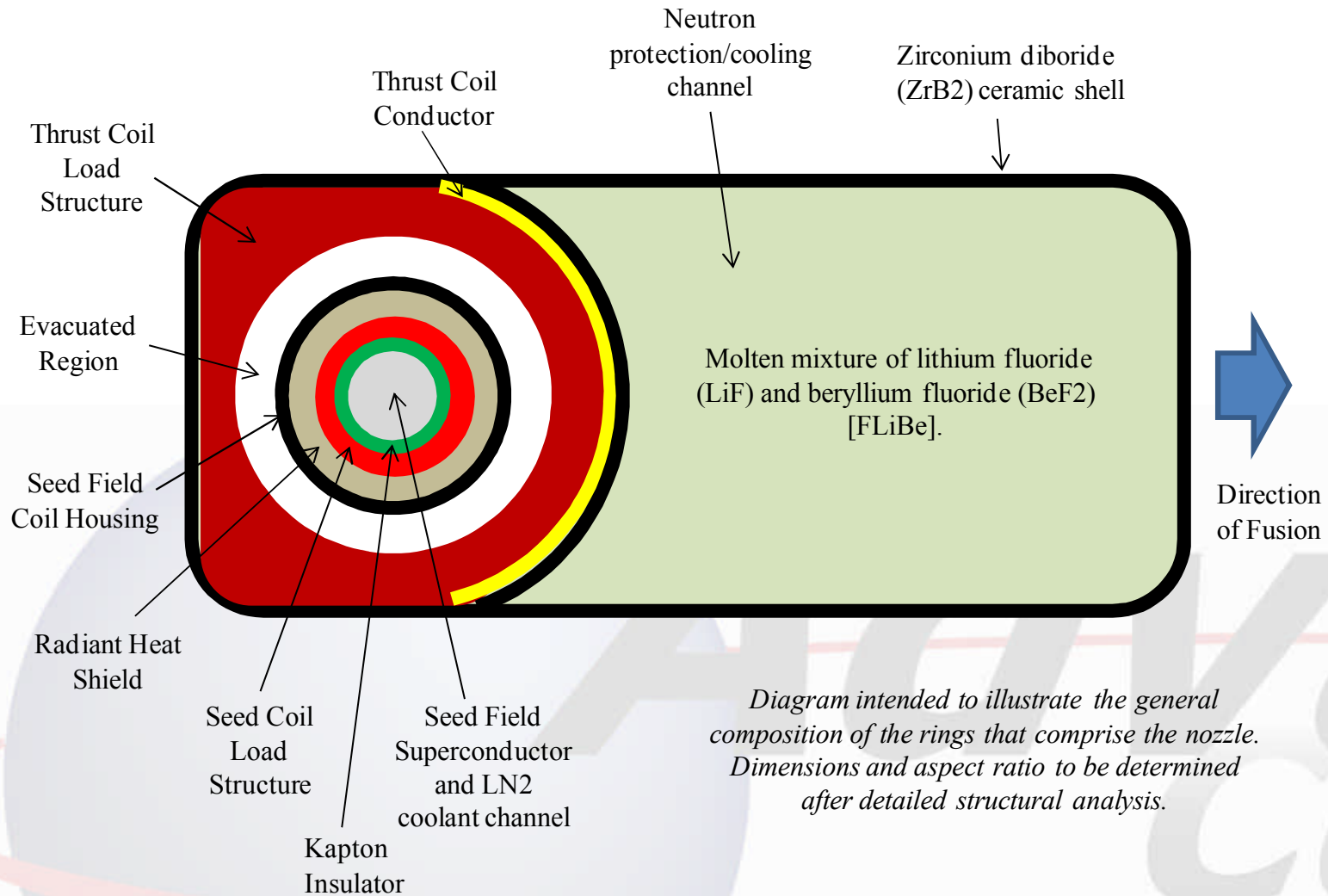
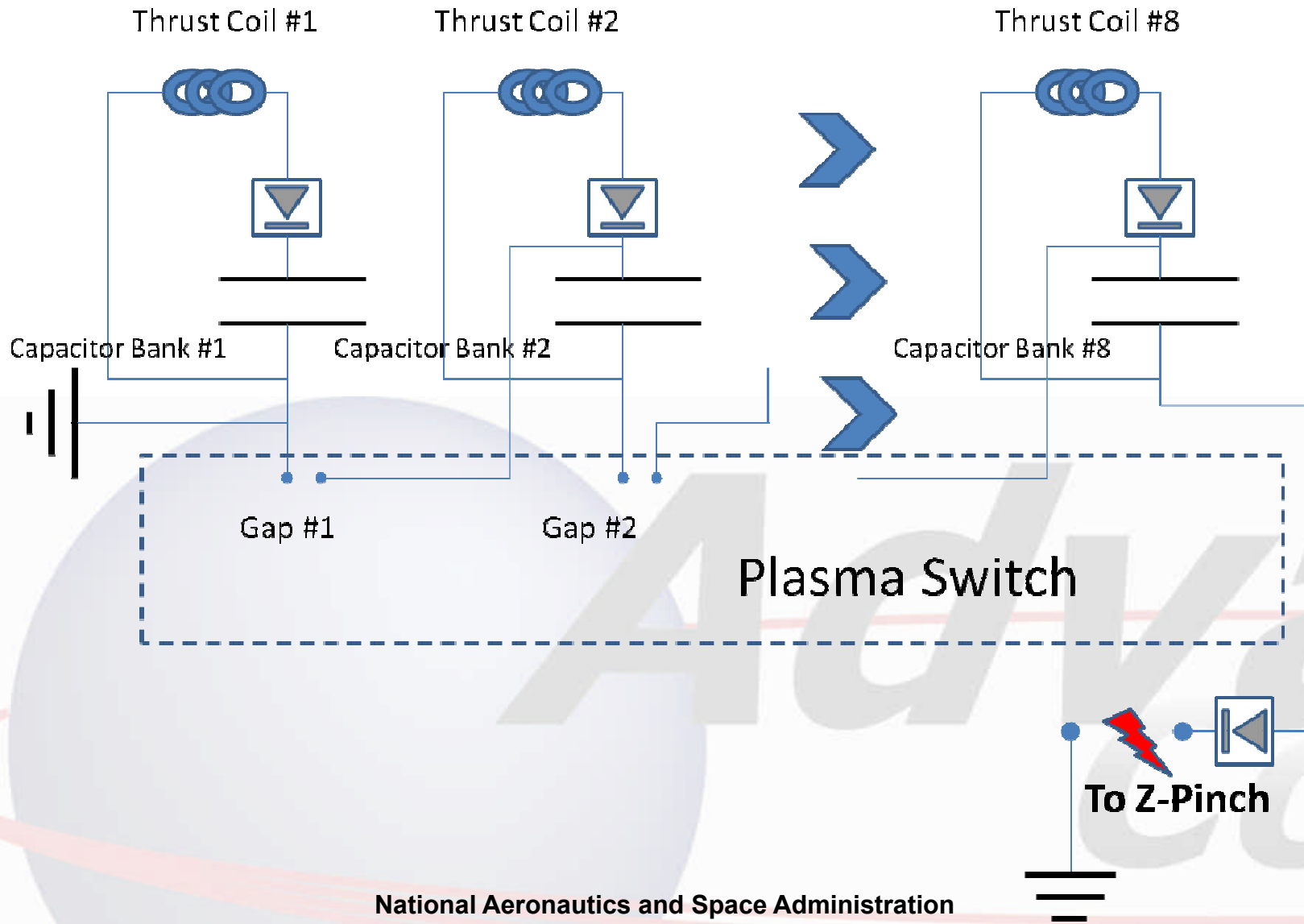


Diagram intended to illustrate the general composition of the rings that comprise the nozzle. Dimensions and aspect ratio to be determined after detailed structural analysis.

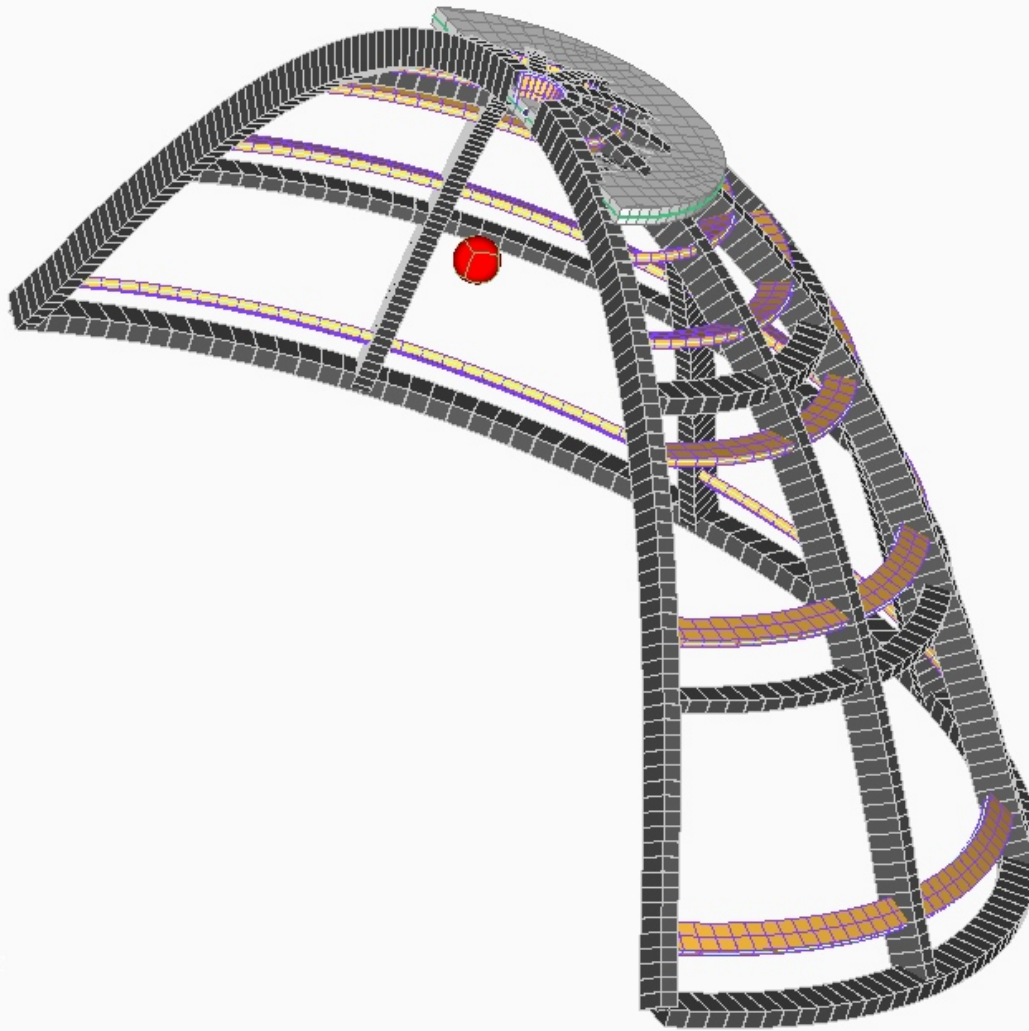


Power Management System





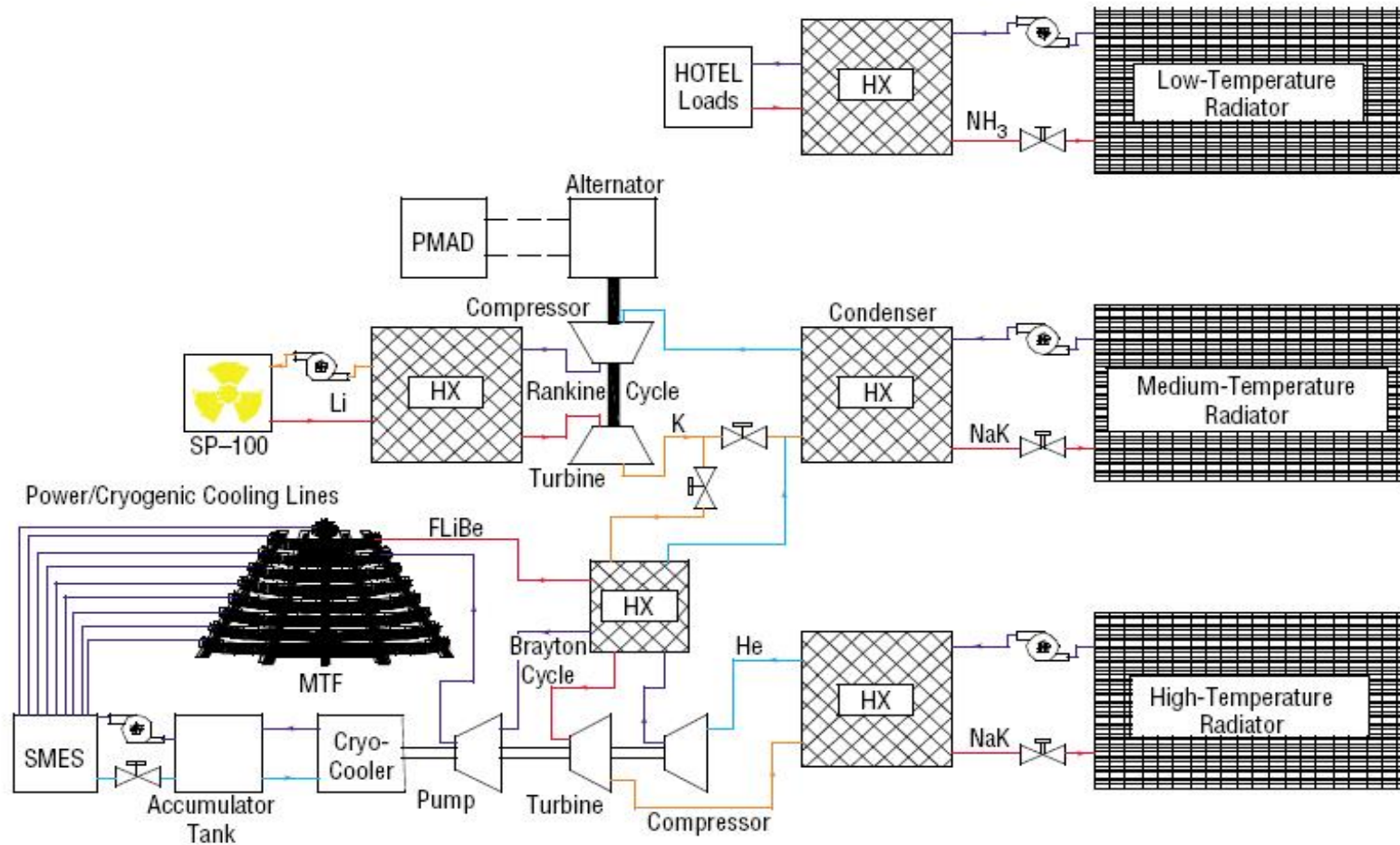
Structural Analysis of Magnetic Nozzle



National Aeronautics and Space Administration
George C. Marshall Space Flight Center
ED04/Advanced Concepts Office

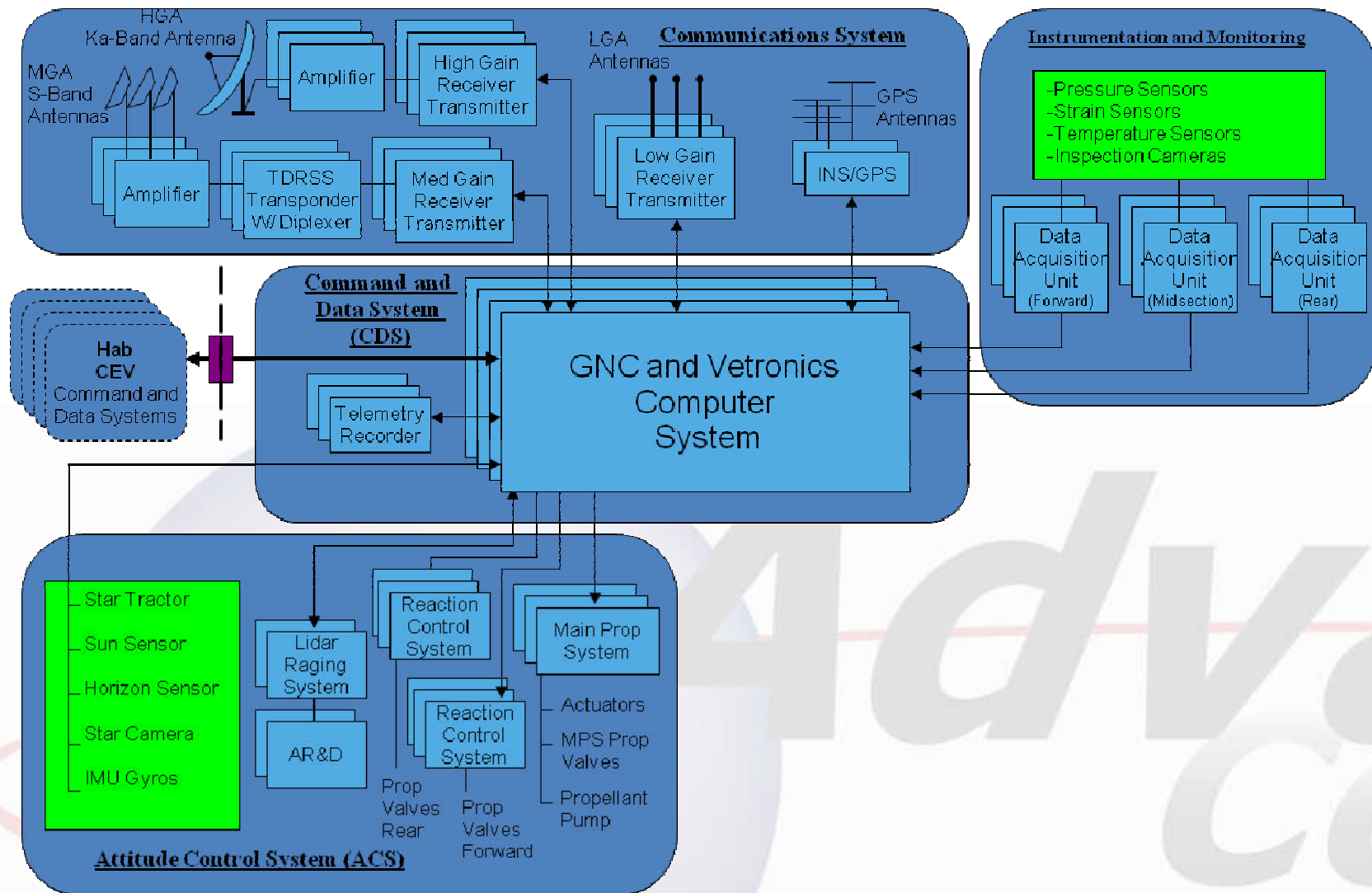


Thermal Management System

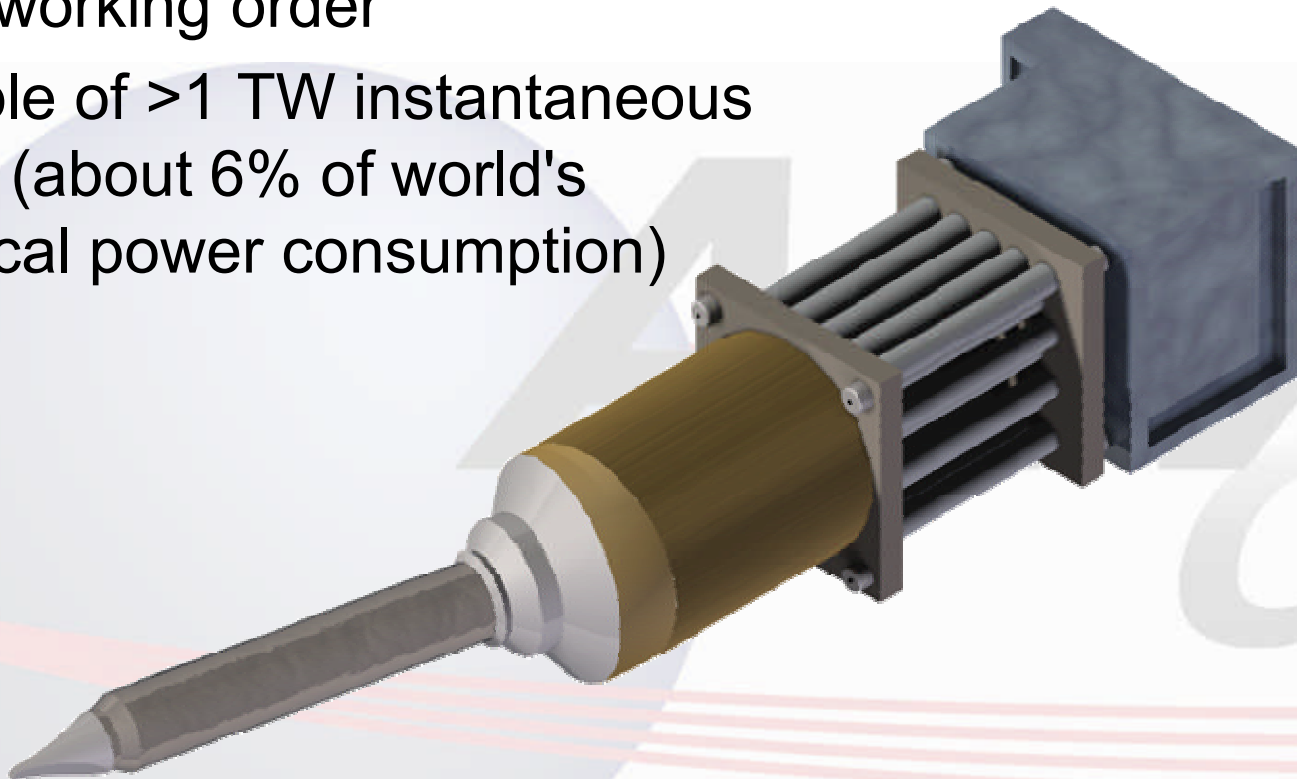




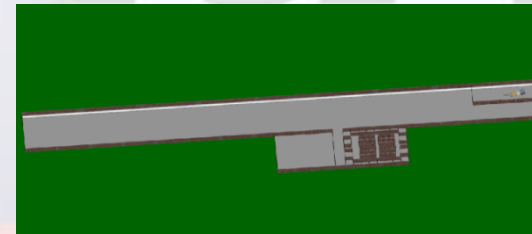
Avionics Suite



- 500 kJ pulsed power facility
- Last prototype built before DECADE construction
- Defense Threat Reduction Agency
 - Nuclear Weapons Effects (NWE)
 - Plasma Radiation Sources (PRS)
- Good working order
- Capable of >1 TW instantaneous power (about 6% of world's electrical power consumption)



- DM2 Utilization Arrangements
 - L3 Communications, Pulsed Science Division
 - Boeing
 - Oak Ridge National Labs
- Other fusion collaborations
 - LANL
 - HyperV Corp.
 - Univ. of New Mexico
- Expected Capabilities
 - 500 ns pulse, 2 MA current
 - 1 keV, 10^{25} /m³ plasma state
 - Effective dwell time of ~100 ns



Aerophysics
lab